

W cross section tension verification using S16-19:

1.1.1 Description

The test verifies the tension strength of W shape section column.

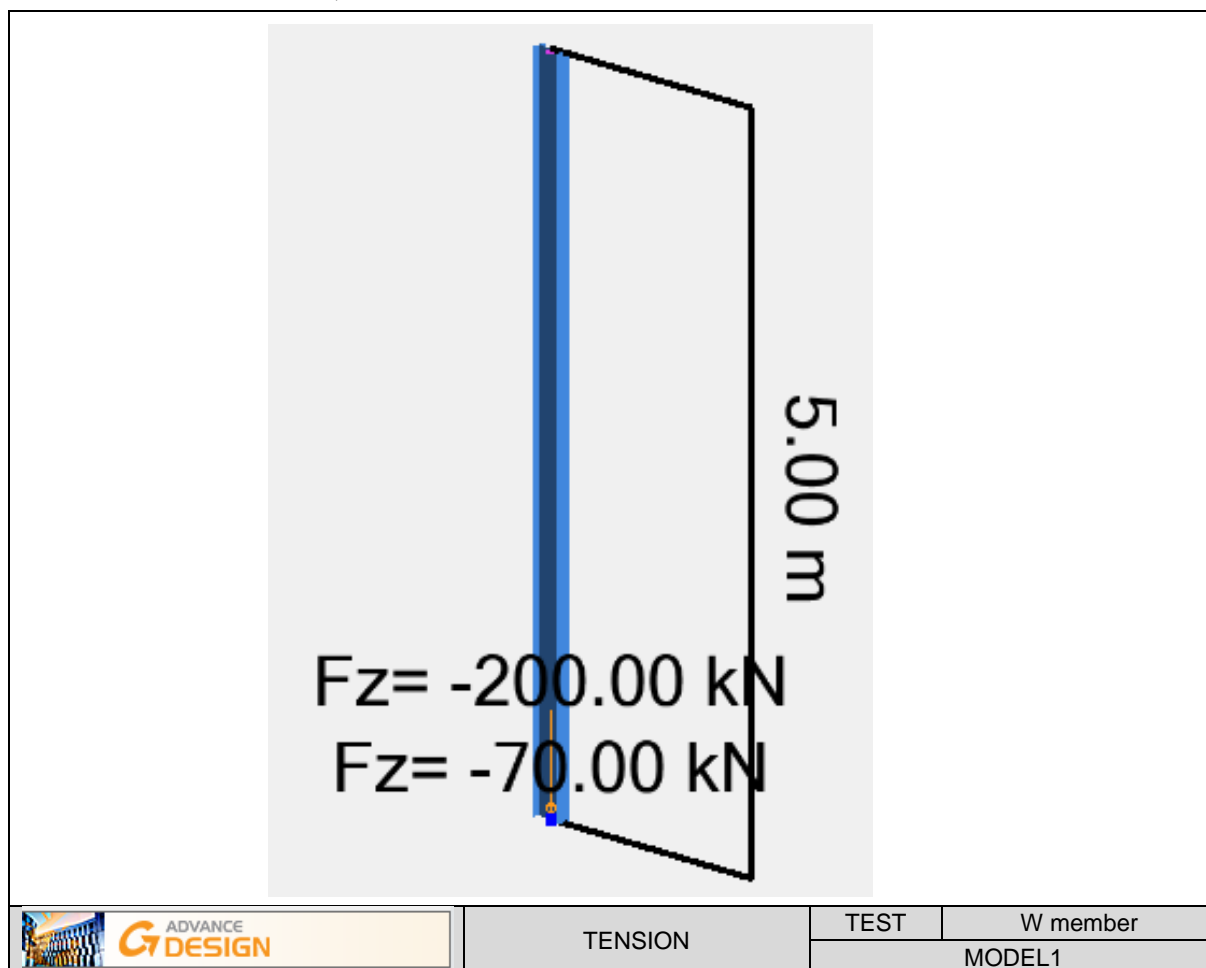
The column is subjected to end tension.

1.1.2 Background

The test verifies the available tension strength of a W250x22 column shown in the figure below. The column is subjected to tension of 70 kN from dead load and 200 kN from live load. Material G40.21M-350W ($F_y=350$ MPa) steel is selected for this example.

1.1.2.1 Model description

- Analysis type: static linear (plane problem)
- Element type: linear
- The following load case is used:
- Load cases: $F_D = -70$ kN; $F_L = -200$ kN

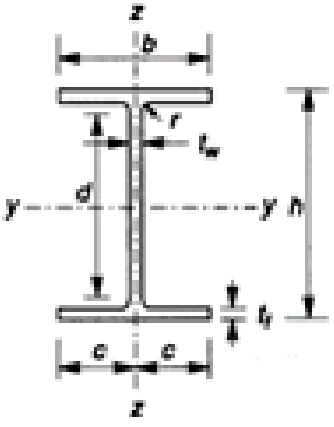


Units

Metric System

Geometry

- Cross section:

<u>Dimensions and surface area</u>		<u>Properties</u>		
	Area		Strong Axis (Y-Y)	
	A	28.50 cm ²	I_y	2870 cm ⁴
	Depth		S_y	226 cm ³
	h	25.4 cm	Z_y	262 cm ³
	Web thickness		Weak Axis (Z-Z)	
	t_w	0.58cm	I_z	120 cm ⁴
	Flange width		S_z	23.8 cm ³
	b	10.2cm	Z_y	37.7cm ³
	Flange thickness		Shear area	
	t_r	0.58cm	A_y	15.17 cm ²
Flillet radius		A_z	14.73 cm ²	
r	1.31cm	Torsional constant		
		J	6.32 cm ⁴	
		Warping constant		
		C_w	18778.2 cm ⁶	
<u>W250x22</u>				

- Beam length: L =500 cm

Materials properties

Steel G40.21M-350W is used. The following characteristics are used in relation to this material:

- Yield strength $f_y=350$ MPa
- Longitudinal elastic modulus: $E=200000$ MPa
- Shear modulus of rigidity: $G=76923.1$ MPa

Boundary conditions

The boundary conditions are described below:

- Outer:
 - ▶ Support at X = 500 cm (Restrains: TX, TY, TZ, Rx, Ry, Rz)
- Inner: None.

Loading

The column is subjected to the following load combinations and actions:

- ULS: $q = 1.25 \times D + 1.5 \times L$
- LSS: $q = 1 \times D + 1 \times L$

1.1.2.2 Reference results in calculating

Reference solution

From the NBC 2015, the required tension strength for the design is:

ULS
$ Fx = 1.25 \times 70 + 1.5 \times 200$ $ Fx = 387.5 \text{ kN}$

The Factored tensile resistance T_r of a member subjected to axial tension is computed from the clause 13.2:

$$T_r = \phi \times A_g \times F_y$$

In order to verify the plasticity of the gross section with the factored load computed at ULS:

ULS
$\phi = 0.9$ $T_r = \phi \times A_g \times F_y = 0.9 \times 2850 \times 350$ $= 897.75 \text{ kN}$ $T_f = Fx = 387.5 \text{ kN} < T_r = 897.75 \text{ kN} \text{ O.K}$ Work ratio: $r = \frac{T_f}{T_r} = 43\%$

Since the member is under tension forces only the verification of bending resistance and combined forces is unnecessary.

Finite elements modeling

- Linear element: S beam,
- 6 nodes,
- 1 linear element.

1.1.2.3 Results comparison

Result name	Result description	Reference value	AD value	Percent Difference
T_r	Factored tensile resistance	897.75 kN	897.75 kN	0.00%
r	Design ratio	43.32%	43%	0.0032%

Cross section | Deflections 0 | Cross Sections Strength (43%) | Class |

	Unfavorable case	Verification	Work ratio
Tension Compression	n°102	$C_f \leq C_r$ (13.2) 387.50 < 897.75 kN	43%
Combined forces	n°102	$M_f/M_r - (T^*Z)/(M_r^*A) \leq 1$ (13.9.2.a) 0.432 < 1.000	43%



Tension

TEST

W section

Model 1



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